

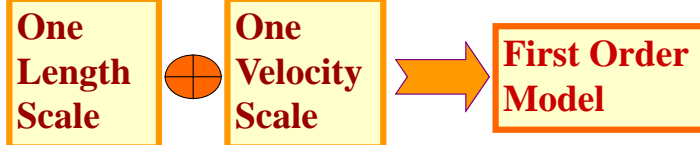
# Turbulence Modeling

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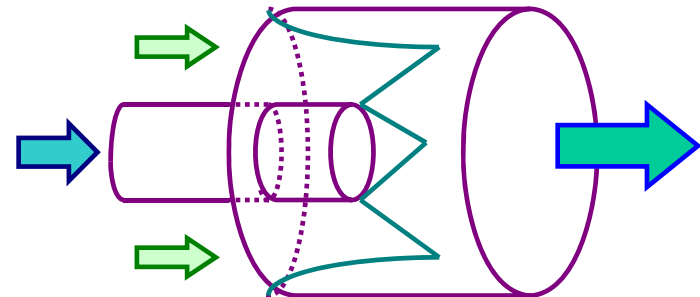
## Outline

- Introduction to Turbulence Modeling
- Eddy Viscosity Models
- Prandtl Mixing Length Model
- One Equation Model
- Two-Equation Model
- $k$ - $\epsilon$  Model
- Stress Transport Model



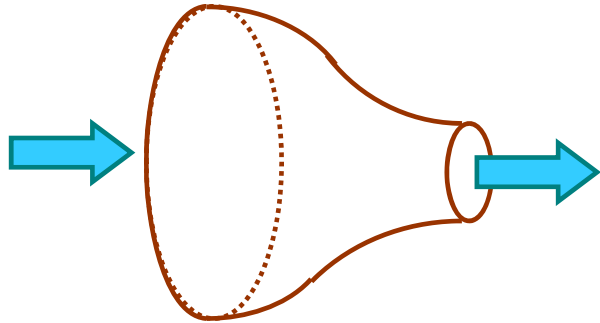
When turbulence is not characterized by one scale, second order modeling has to be used.

## Example of Multi-Scale Flows



## Two-Equation Turbulence Models Clarkson University

### Example of Accelerated Flows



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## Prandtl-Kolmogorov Equation Clarkson University

Eddy Viscosity



$$v_T = k^2 \ell$$

Second Scale of turbulence



$$z = k^m \ell^n$$

Kolmogorov

$$f = \frac{k^2}{\ell} \quad m = \frac{1}{2} \quad n = -1$$

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## Examples of z-Expression Clarkson University

Laufer-Spalding



$$\varepsilon = \frac{k^{\frac{3}{2}}}{\ell} \quad m = \frac{3}{2} \quad n = -1$$

Rotta



$$k\ell \quad m = 1 \quad n = 1$$

Rotta



$$\ell \quad m = 0 \quad n = 1$$

Spalding



$$w = \frac{k}{\ell^2} \quad m = 1 \quad n = -2$$

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## Thin Shear Layer Two-Equation Model Clarkson University

$$\frac{dk}{dt} = \frac{\partial}{\partial y} \left( \frac{v_T}{\sigma_k} \frac{\partial k}{\partial y} \right) + k \left[ \frac{v_T}{k} \left( \frac{\partial U}{\partial y} \right)^2 - c_D \frac{k}{v_T} \right]$$

$$\frac{dz}{dt} = \frac{\partial}{\partial y} \left( \frac{v_T}{\sigma_z} \frac{\partial z}{\partial y} \right) + z \left[ C_1 \frac{v_T}{k} \left( \frac{\partial U}{\partial y} \right)^2 - C_2 \frac{k}{v_T} \right] + \frac{s_z}{\rho}$$

$$\sigma_z, C_1, C_2 \sim \text{Const.}$$

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## Evaluation of Constants - Decaying Turbulence Clarkson University

Decay Behind a Grid

$$k \sim X^{-1}$$

k-Eq.

$$U_0 \frac{dk}{dx} = -C_D \frac{k^2}{v_T}$$

z-Eq.

$$U_0 \frac{dz}{dx} = -C_2 \frac{kz}{v_T}$$

$$C_2 = C_D \left( m - \frac{n}{2} \right)$$

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## Evaluation of Constants - Inertial Sublayer Clarkson University

$$\ell = \kappa y$$

$$k = C_D^{-\frac{1}{2}} u^{*2}$$

$$v_T = C_D^{-\frac{1}{2}} \kappa u^* y$$

$$z = k^m \ell^n = C_D^{-\frac{m}{2}} u^{*2m} (\kappa y)^n = A y^n$$

k-Eq.

$$\frac{v_T}{k} \left( \frac{\partial U}{\partial y} \right)^2 - C_D \frac{k}{v_T} = 0$$

z-Eq.

$$\frac{\partial}{\partial y} \left( \frac{v_T}{\sigma_z} \frac{\partial z}{\partial y} \right) + z \left[ C_1 \frac{v_T}{k} \left( \frac{\partial U}{\partial y} \right)^2 - C_2 \frac{k}{v_T} \right] = 0$$

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## Evaluation of Constants - Inertial Sublayer Clarkson University

Eliminating U

$$\frac{\partial}{\partial y} \left( \frac{v_T}{\sigma_z} \frac{\partial z}{\partial y} \right) + \frac{zk}{v_T} (C_1 C_D - C_2)$$

z-Eq.

$$C_1 = \frac{C_2}{C_D} - \frac{\kappa^2 n^2}{\sigma_z C_D}$$

ε-Eq.

$$C_2 = 2C_D$$

$$C_1 = 2 - \frac{\kappa^2}{\sigma_z C_D}$$

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## z-Equations Clarkson University

$$\frac{D}{Dt} (k\ell) = \frac{\partial}{\partial y} \left( \frac{v_T}{\sigma_{k\ell}} \frac{\partial (k\ell)}{\partial y} \right) + 0.98k^{\frac{1}{2}} \ell^2 \left( \frac{\partial U}{\partial y} \right)^2 - 0.059k^{\frac{3}{2}} - \left[ 702 \left( \frac{\ell}{y} \right)^6 k^{\frac{3}{2}} \right]$$

For Near Wall Flows

$$\frac{D}{Dt} W = \frac{\partial}{\partial y} \left( \frac{v_T}{\sigma_w} \frac{\partial W}{\partial y} \right) + 1.04W^{\frac{1}{2}} \left( \frac{\partial U}{\partial y} \right)^2 - 0.17W^{\frac{3}{2}} + 3.5v_T \left( \frac{\partial^2 U}{\partial y^2} \right)^2$$

$$\frac{D}{Dt} \varepsilon = \frac{\partial}{\partial y} \left( \frac{v_T}{\sigma_\varepsilon} \frac{\partial \varepsilon}{\partial y} \right) + 1.45k \left( \frac{\partial U}{\partial y} \right)^2 - 0.18 \frac{\varepsilon^2}{k}$$

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# Boundary Conditions Clarkson University

Plan of Symmetry



$$\frac{\partial k}{\partial y} = 0$$

$$\frac{\partial z}{\partial y} = 0$$

Free Surface

$$U_0 \frac{dk_0}{dx} = c_D \frac{k_0^2}{v_{T0}}$$

$$\frac{\partial k_0}{\partial y} = 0$$

$$U_0 \frac{dz_0}{dx} = c_z \frac{k_0 z_0}{v_{T0}}$$

$$\frac{\partial z_0}{\partial y} = 0$$

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# Boundary Conditions Clarkson University

Near a Wall

$$U^+ = \frac{1}{\kappa} \ln y^+ + C$$

$$k^+ = C_D^{-\frac{1}{2}}$$

$$z^+ = C_D^{\frac{1}{2}(\frac{n}{2}-m)} (\kappa y^+)^n$$

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# Two-Equation Model Clarkson University

**k-ε Model**

Exact k-equation

$$\frac{dk}{dt} = -\frac{\partial}{\partial x_i} \left[ u'_i \left( \frac{1}{2} u'_j u'_j + \frac{P'}{\rho} \right) \right] - \overline{u'_i u'_j} \frac{\partial U_i}{\partial x_j} - \varepsilon + \nu \nabla^2 k$$

Exact ε-equation up to order  $\left(\frac{u^3}{\lambda \lambda^2}\right)$

$$\varepsilon = \nu \overline{\omega'_i \omega'_i}$$

$$\frac{d}{dt} \left( \frac{1}{2} \overline{\omega'_i \omega'_i} \right) = -\frac{1}{2} \frac{\partial}{\partial x_j} \left( \overline{u'_j \omega'_i \omega'_i} \right) + \overline{\omega'_i \omega'_j} d'_{ij} - \nu \frac{\partial \omega'_i}{\partial x_j} \frac{\partial \omega'_i}{\partial x_j}$$

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# Two-Equation k-e Model Clarkson University

$$-\overline{u'_i u'_j} = \nu_T \left( \frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right) - \frac{2}{3} k \delta_{ij}$$

$$\nu_T = C_\mu \frac{k^2}{\varepsilon}$$

$$-\overline{u'_i \left( \frac{1}{2} u'_j u'_j + \frac{P'}{\rho} \right)} = \frac{\nu_T}{\sigma_k} \frac{\partial k}{\partial x_i}$$

**Modeled k-Equation**

$$\frac{dk}{dt} = \frac{\partial}{\partial x_i} \left( \frac{\nu_T}{\sigma_k} \frac{\partial k}{\partial x_i} \right) + \nu_T \left( \frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right) \frac{\partial U_i}{\partial x_j} - \varepsilon$$

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# Two-Equation Model Clarkson University

## Modeling $\varepsilon$ -Equation

**Diffusion**  $\rightarrow$  
$$-\overline{v u'_j \omega'_i \omega'_i} = \frac{v_T}{\sigma_\varepsilon} \frac{\partial \varepsilon}{\partial x_j}$$

**Production** 
$$2v \overline{\omega'_i \omega'_j d'_{ij}} = c_{\varepsilon 1} \frac{\varepsilon}{k} v_T \left( \frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right) \frac{\partial U_i}{\partial x_j}$$

**Dissipation**  $\rightarrow$  
$$2v^2 \frac{\partial \omega'_i}{\partial x_j} \frac{\partial \omega'_i}{\partial x_j} = c_{\varepsilon 2} \frac{\varepsilon^2}{k}$$

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# Two-Equation Model Clarkson University

## $\varepsilon$ -Equation

$$\frac{d\varepsilon}{dt} = \frac{\partial}{\partial x_j} \left( \frac{v_T}{\sigma_\varepsilon} \frac{\partial \varepsilon}{\partial x_j} \right) + c_{\varepsilon 1} v_T \frac{\varepsilon}{k} \left( \frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right) \frac{\partial U_i}{\partial x_j} - c_{\varepsilon 2} \frac{\varepsilon^2}{k}$$

$$c_\mu = 0.09$$

$$c_{\varepsilon 1} = 1.45$$

$$c_{\varepsilon 2} = 1.9$$

$$\sigma_k = 1$$

$$\sigma_\varepsilon = 1.3$$

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# Boundary Conditions Near a Wall Clarkson University

## At a first Grid P

$\dot{P}$

$$\frac{U_P}{u_*^2} C_\mu^{1/4} k_P^{1/2} = \frac{1}{\kappa} \ln \left[ E y_P \frac{(C_\mu^{1/2} k_P)^{1/2}}{v} \right]$$

$$\int_0^{y_P} \varepsilon dy = C_\mu \frac{k_P^{3/2}}{\kappa} \ln \left[ \frac{E y_P (C_\mu^{1/2} k_P)^{1/2}}{v} \right]$$

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# Low Reynolds Number Models Clarkson University

## Jones-Launder

$$\frac{Dk}{Dt} = \frac{\partial}{\partial x_i} \left[ \left( v + \frac{v_T}{\sigma_k} \right) \frac{\partial k}{\partial x_i} \right] + P - \hat{\varepsilon} \quad P = -\overline{u'_i u'_j} \frac{\partial U_i}{\partial x_j}$$

$$\frac{D\varepsilon}{Dt} = \frac{\partial}{\partial x_i} \left[ \left( v + \frac{v_T}{\sigma_\varepsilon} \right) \frac{\partial \varepsilon}{\partial x_i} \right] + c_{\varepsilon 1} \frac{\hat{\varepsilon}}{k} P + 2v v_T \left( \frac{\partial^2 U_i}{\partial x_j \partial x_k} \right)^2 - c_{\varepsilon 2} \frac{\hat{\varepsilon}^2}{k}$$

$$\overline{u'_i u'_j} = \frac{2}{3} \delta_{ij} k - v_T \left( \frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right)$$

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## Low Reynolds Number Models Clarkson University

### Jones-Launder

$$v_T = c_\mu \frac{k^2}{\varepsilon}$$

$$\hat{\varepsilon} = \varepsilon - 2v \left( \frac{\partial \sqrt{k}}{\partial x_j} \right)^2$$

$$c_\mu = 0.09 \exp \left\{ -\frac{2.51}{(1 + R_T/50)} \right\}$$

$$R_T = \frac{k^2}{v\varepsilon}$$

$$c_{\varepsilon 2} = 1.9 [1 - 0.3 \exp(-R_T^2)]$$

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## Low Reynolds Number Models Clarkson University

### Saffman Model

$$v_T = \frac{Ak}{W}$$

$$\frac{D}{Dt} k = \alpha'' k (2S_{ij}^2)^{\frac{1}{2}} - kW + A'' \frac{\partial}{\partial x_j} \left( \frac{k}{W} \frac{\partial k}{\partial x_j} \right)$$

$$\frac{D}{Dt} W^2 = \alpha' W^2 [\eta U_{i,j}^2 + 2(1-\eta) S_{ij}^2]^{\frac{1}{2}} - \beta' W^3 + A' \frac{\partial}{\partial x_j} \left( \frac{k}{W} \frac{\partial W^2}{\partial x_j} \right)$$

$$\beta' = \frac{5}{3}$$

$$A = \Gamma^2$$

$$\alpha'' = \Gamma$$

$$\Gamma = \frac{u^{*2}}{k} \approx 0.3$$

$$\eta = 1$$

$$\alpha' = \frac{\beta' \alpha'' - 4A' k^2}{A}$$

$$A' = A'' = \frac{1}{2} A$$

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## Low Reynolds Number Models Clarkson University

### K- $\omega$ Model

$$\rho U \frac{\partial U}{\partial x} + \rho V \frac{\partial U}{\partial y} = \frac{\partial}{\partial y} \left[ (v + v_T) \frac{\partial U}{\partial y} \right]$$

$$v_T = \frac{\alpha^* k}{\omega}$$

$$U \frac{\partial k}{\partial x} + V \frac{\partial k}{\partial y} = v_T \left( \frac{\partial U}{\partial y} \right)^2 - \beta^* \omega k + \frac{\partial}{\partial y} \left[ (v + \sigma^* v_T) \frac{\partial k}{\partial y} \right]$$

$$U \frac{\partial \omega}{\partial x} + V \frac{\partial \omega}{\partial y} = \alpha \frac{\omega}{k} v_T \left( \frac{\partial U}{\partial y} \right)^2 - \beta \omega^2 + \frac{\partial}{\partial y} \left[ (v + \sigma \mu_T) \frac{\partial \omega}{\partial y} \right]$$

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## Stress Transport - Boundary Layer Clarkson University

### Exact Transport Equation

$$\begin{aligned} \frac{D}{Dt} \overline{u'v'} = & \underbrace{-\overline{v'^2} \frac{\partial U}{\partial y}}_{\text{Production}} - \underbrace{\frac{\partial}{\partial y} \left( \overline{u'v'^2} - \frac{P'u'}{\rho} \right)}_{\text{Diffusion}} \\ & + \underbrace{\frac{P'}{\rho} \left( \frac{\partial u'}{\partial y} + \frac{\partial u'}{\partial x} \right)}_{\text{Pressure-Strain}} - \underbrace{2v \frac{\partial u'}{\partial x_k} \frac{\partial v'}{\partial x_k}}_{\text{Dissipation}} \end{aligned}$$

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## Stress Transport Model (Hanjalic) Clarkson University

$$\text{Production} \approx k \frac{\partial U}{\partial y}$$

$$\text{Diffusion} \approx \frac{\partial}{\partial y} \left[ \frac{\nu_T}{\sigma_T} \frac{\partial \overline{u'v'}}{\partial y} \right]$$

$$\text{Dissipation} \approx 0$$

$$\text{Pressure-strain} \approx \frac{k^2}{\ell} \overline{u'v'}$$

### Modeled Equation

$$\frac{D}{Dt} \overline{u'v'} = \frac{\partial}{\partial y} \left[ \frac{\nu_T}{\sigma_z} \frac{\partial \overline{u'v'}}{\partial y} \right] - c_\tau \left( k \frac{\partial U}{\partial y} + \frac{k^2}{\ell} \overline{u'v'} \right)$$

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## Second-Order Turbulence Models Clarkson University

### Concluding Remarks

- Two Equation Models
- k-ε Model
- Stress Transport Models
- Algebraic Stress Models

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## Turbulence Models Clarkson University

# Thank you!

# Questions?

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