

Turbulence Deposition

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Outline

- ▶ Semi-Empirical Models
- ▶ Free Flight Models
- ▶ Flow Structure Models
- ▶ Sublayer/Burst Models
- ▶ Deposition on Rough Walls

Papavergos and Hedely (1984)

Vertical Channel

$$\tau^+ < 0.2$$

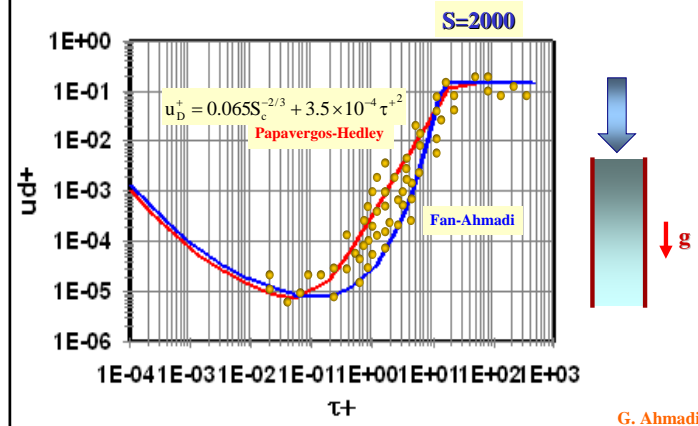
$$u_D^+ = 0.065 S_c^{-2/3}$$

$$0.2 < \tau^+ < 20$$

$$u_D^+ = 3.5 \times 10^{-4} \tau^{+2}$$

$$\tau^+ > 20$$

$$u_D^+ = 0.18$$



Turbulence Deposition Velocity Clarkson University

Papavergos and Hedely (1984)

Horizontal Duct

Floor

$0.2 < \tau^+ < 20$

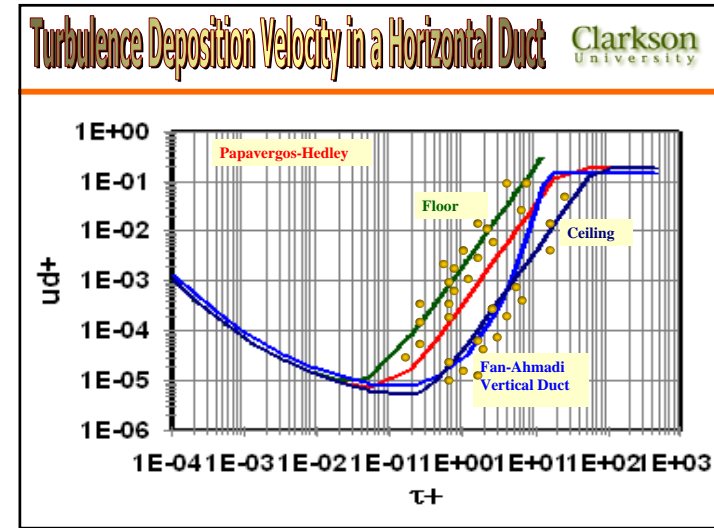
$u_D^+ = 2 \times 10^{-3} \tau^{+2}$

Ceiling

$0.2 < \tau^+ < 20$

$u_D^+ = 4 \times 10^{-5} \tau^{+2}$

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Turbulence Deposition Theories Clarkson University

Mass Flux

$J = (D + D^T) \frac{\partial C}{\partial y}$

→

$u_D^+ = (D^+ + D^{T+}) \frac{\partial C^+}{\partial y^+}$

Deposition Velocity

 $u_D^+ = \frac{u_D}{u^*} = \frac{1}{u^*} \left(\frac{J}{C_0} \right)$

$C^+ = \frac{C}{C_0}$

$D^T = v^T$

$D^{T+} = v^{T+}$

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Friedlander and Johnstone Model (Free Flight) Clarkson University

Eddy Diffusivity

Friedlander and Johnstone (1959)

$D^{T+} = v^{T+} = \begin{cases} \left(\frac{y^+}{14.5}\right)^3 & 0 \leq y^+ \leq 5 \\ \frac{y^+}{5} - 0.959 & 5 \leq y^+ \leq 30 \end{cases}$

$C\left(s^+ + \frac{d^+}{2}\right) = 0$

Stopping Distance

$s = U_f \tau$

Free Flight Velocity

 $U_f = 0.9u^* = 0.9\bar{U} \sqrt{\frac{f}{2}}$

$f = C_f = \frac{\tau_0}{0.5\rho U^2}$

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Friedlander and Johnstone Model Clarkson University

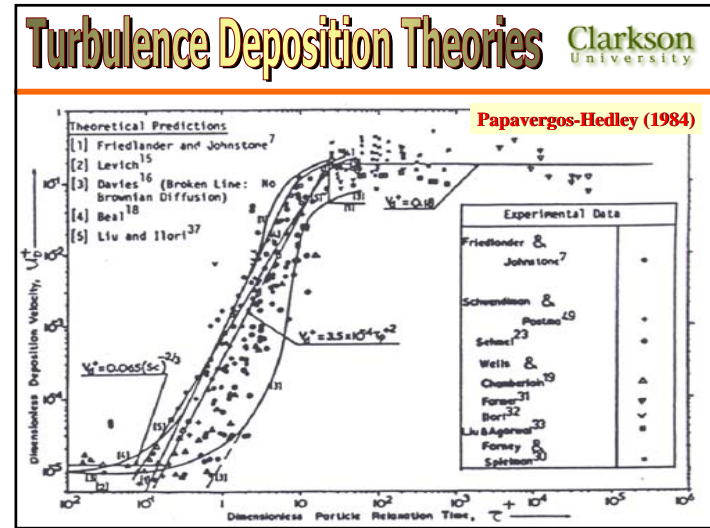
Deposition Velocity $s^+ = 0.9\tau^+$

$u_d^+ = \left(\frac{1}{\sqrt{f/2}} + \frac{1525}{s^{+2}} - 50.6 \right)^{-1}$ $s^+ \leq 5$

$u_d^+ = \left[\frac{1}{\sqrt{f/2}} - 13.75 + 5 \ln \left(\frac{5.04}{0.5s^+ - 0.959} \right) \right]^{-1}$ $5 \leq s^+ \leq 30$

$u_d^+ = \sqrt{f/2}$ $s^+ \geq 30$

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Free Flight Deposition Models Clarkson University

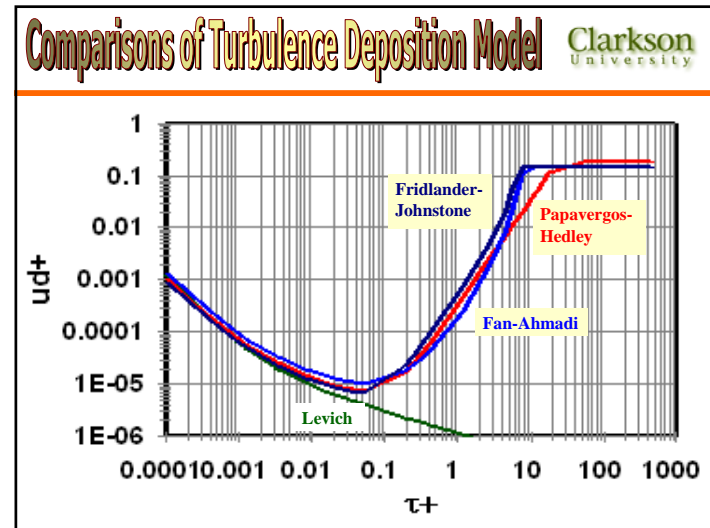
Levich (1962) $v^T \sim y^{+4}$ $u_D^+ = 0.13337S_c^{-3/4}$

Davies $u_D^+ = 0.057s_c^{-2/3}$

Schmel $D^{T+} = 0.011(y^+)^{-1}(\tau^+)^{-1} \quad y^+ < 20$ $U_f^+ = 1.49(\tau^+)^{-0.49}$
 $D^{T+} = 0.04y^+ \quad y^+ > 20$

Liu and Ilory $D^{T+} = v^{T+} + \left(\frac{y^+}{y^+ + 10} \right)^2 \tau^+$

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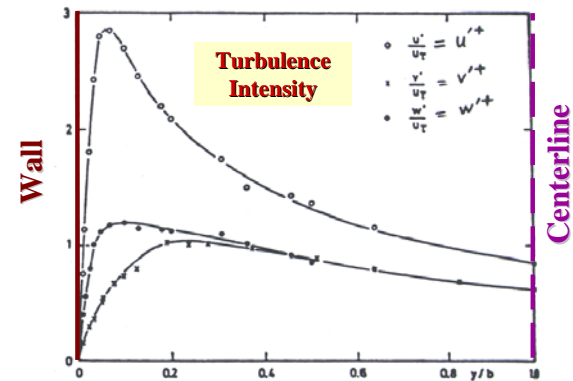
Limitations of Free-Flight Models Clarkson University

- Use of the concept of 'stopping distance' as a sink boundary condition for particle
- Assumptions for free-flight velocity
- Equality of particle mass diffusivity to the turbulence eddy diffusion.
- Ignoring the effects of density ratio, Reynolds number, and scales of turbulence.
- Ignoring the effects of lift force.
- Ignoring the effects of coherent eddies and bursting phenomena.

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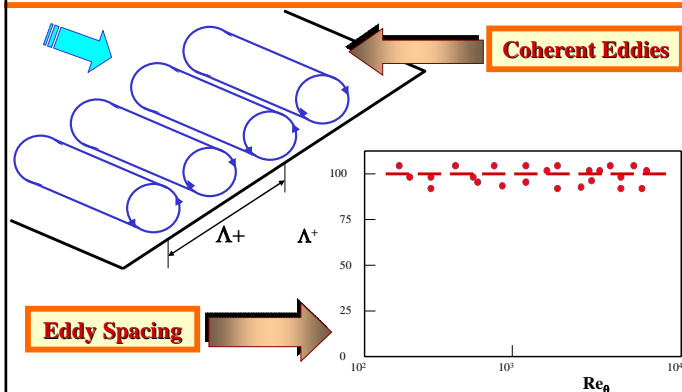
Structure of Turbulence Near a Wall Clarkson University



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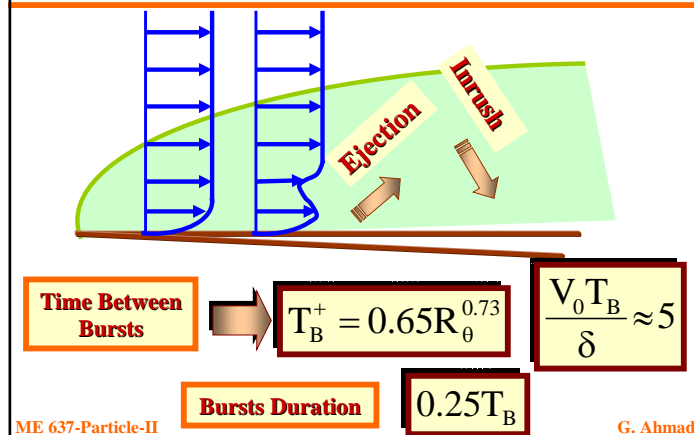
Streaky Wall Flow Clarkson University



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Bursting Phenomena Clarkson University



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Cleaver and Yates Model Clarkson University

- Suspended particles diffuse to a certain distance from the wall by turbulent diffusion before being entrained in a down-sweep.
- The flow in a down-sweep may be approximated as a two-dimensional stagnation-point flow in the sub-layer.
- Only Stokes drag is acting on the particles.

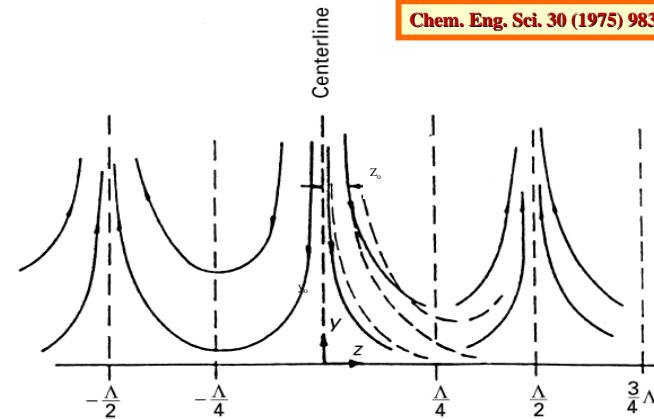
$$u_D^+ = \frac{9}{400} \frac{\rho^f}{\rho^p} \tau^+ \exp\{0.48\tau^+\} + 0.084Sc^{-2/3}$$

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Cleaver-Yates Model Clarkson University

Chem. Eng. Sci. 30 (1975) 983.



Cleaver and Yates Model Clarkson University

Flux

$$J = C(y)v_0(y)A_c(y)$$

Deposition Velocity

$$u_D^+ = \frac{J}{Cu^*} = \frac{v_0^+ A_c}{2}$$

Equation of Motion

$$A_c - \text{capture area ratio} = \frac{z_0}{\Lambda}$$

$$\tau^+ \frac{dv^+}{dt^+} = v^{f+} - v^+$$

$$\tau^+ \frac{dw^+}{dt^+} = w^{f+} - w^+$$

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Cleaver and Yates Model Clarkson University

Perturbation Solution

$$v^+ = v^{f+} - \tau^+ \left(v^{f+} \frac{\partial v^{f+}}{\partial y^+} + w^{f+} \frac{\partial v^{f+}}{\partial z^+} \right)$$

$$w^+ = w^{f+} - \tau^+ \left(v^{f+} \frac{\partial w^{f+}}{\partial y^+} + w^{f+} \frac{\partial w^{f+}}{\partial z^+} \right)$$

Flow Field

$$w^f = \alpha z \varphi'(\eta)$$

$$v^f = -\sqrt{\alpha \nu} \varphi(\eta)$$

$$\eta = \sqrt{\frac{\alpha}{\nu}} y$$

$$\varphi'''' + \varphi \varphi'' - \varphi'^2 + 1 = 0$$

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Cleaver and Yates Model Clarkson University

$\alpha = 0.067 \frac{u^{*2}}{v}$

↔

$y^+ = 10$

↔

$v^{f+} = \frac{1}{2}$

Boundary condition

→

$y^+ = \frac{d^+}{2}$

→

$z^+ = 70$

→

$A_c = \frac{z_0^+}{z^+}$

Limiting Trajectory

→

$$\ln \frac{z^+}{z_0^+} = \int_{\frac{\alpha v}{u^2} y_0^+}^{\frac{\alpha v}{u^2} y^+} \left\{ \frac{\phi' - \tau^+ \left(\frac{\alpha v}{u^2} \right) (\phi'^2 - \phi \phi'')}{\phi + \tau^+ \left(\frac{dv}{u^2} \right) \phi \phi'} \right\} dy$$

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Cleaver and Yates Model Clarkson University

Deposition Velocity

↔

$u_D^+ = \frac{9}{400} \frac{\rho^f}{\rho^p} \tau^+ \exp\{0.48\tau^+\}$

↔

$\tau^+ \ll 1$

$u_D^+ = 0.45 \exp\left\{-\frac{\tau^+}{0.9} \int_{d^+/2}^{\infty} \left(1 - \frac{f(y)}{0.9}\right) dy\right\}$

↔

$\tau^+ \gg 1$

To Account for Convection

→

$u_D^+ = 8.5 A_c$

Deposition Velocity, Diffusion

↔

$u_D^+ = 0.084 S_c^{-2/3}$

Minimum Deposition Velocity

→

$\tau^+ S_c^{2/3} = 0.069 \frac{\rho_p}{\rho_f}$

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Fichman et al. Model Clarkson University

Flow Field

$U^+ = y^+$

$$\left. \begin{aligned} v^+ &= B\phi = 0.625B^3 y^{+2} \\ \phi &= 0.625\eta^2, \quad \eta = By^+, \quad B = 0.271 \end{aligned} \right\} \text{for } y^+ \leq 2$$

$$\left. \begin{aligned} v^+ &= c\phi = 0.24c - 0.71c^2 y^+ \\ \phi &= 0.71\eta - 0.24, \quad \eta = cy^+, \quad c = 0.174 \end{aligned} \right\} \text{for } 2 \leq y^+ \leq 7$$

$$\left. \begin{aligned} U^+ &= 0.3y^+ + 0.5 \\ v^+ &= c\phi = 0.6c - c^2 y^+, \quad \phi = \eta - 0.6 \end{aligned} \right\} \text{for } 7 \leq y^+ \leq 30$$

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Fichman et al. Model Clarkson University

Deposition Velocity

$u_D^+ = \frac{1}{2} A_c v_0^+$

$A_c = \frac{Z_{lim}}{\Lambda/4} = \frac{Z_{lim}^+}{\Lambda^+/4}$

$u_D^+ = \frac{2Z_{lim}^+ v_0^+}{\Lambda^+}$

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Fichman et al. Model Clarkson University

Equations of Motion

$$\tau^+ \frac{d^2 x^+}{dt^{+2}} = U^+ - \frac{dx^+}{dt}$$

$$\tau^+ \frac{d^2 y^+}{dt^{+2}} = v^+ - \frac{dy^+}{dt} + K \left(U^+ - \frac{dx^+}{dt} \right)$$

$$\tau^+ \frac{d^2 z^+}{dt^{+2}} = w^+ - \frac{dz^+}{dt} \quad K = \tau^+ L^+$$

Lift

$$L^+ = \frac{Lv}{u^{*2}}$$

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Lift

$$L \approx \frac{6.46\mu \left(\frac{d}{2}\right)^2}{v^{1/2} m_p} \left(\frac{dU}{dy}\right)^{1/2} = \frac{3.08\mu \dot{\gamma}^{1/2}}{v^{1/2} d \rho_p} \quad \dot{\gamma} = \frac{dU}{dy}$$

$$\dot{\gamma} = \frac{dU}{dy}$$

$$\frac{4z_{lim}^+}{\Lambda^+} = \frac{d^2 + (d^+ + s^+)s^+}{4}$$

$$s^+ \leq 2$$

$$s^+ = \frac{L^+ \tau^{+2} (u_{po}^+ - \dot{\gamma}^+ y_0^+) + \tau^+ v_{po}^+}{1 - \tau^{+2} L^+ \dot{\gamma}^+}$$

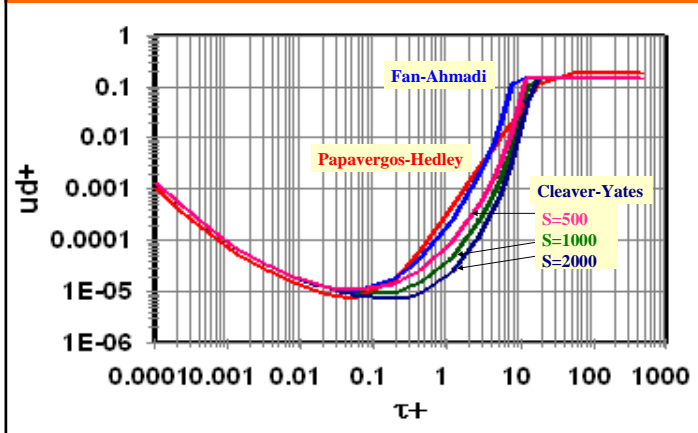
Numerical Solution

$$s^+ \geq 2$$

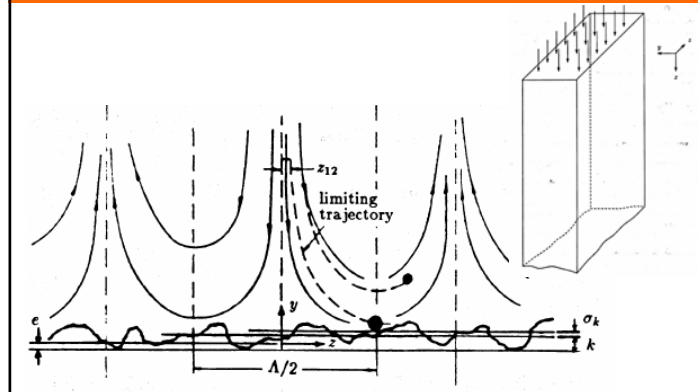
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Cleaver and Yates Model Clarkson University



Fan-Ahmadi Model Clarkson University



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Equations of Motion

$$\tau^+ \frac{du^{p+}}{dt^+} = u^+ - u^{p+} + \tau^+ g^+,$$

$$\tau^+ \frac{dv^{p+}}{dt^+} = v^+ - v^{p+} + \tau^+ L_1^+(u^+ - u^{p+}) + \tau^+ L_2^+(w^+ - w^{p+}),$$

$$\tau^+ \frac{dw^{p+}}{dt^+} = w^+ - w^{p+},$$

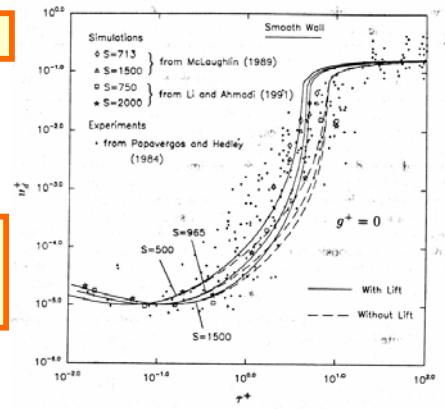
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Fan-Ahmadi Model Clarkson University

Smooth Wall

Comparison with Simulations



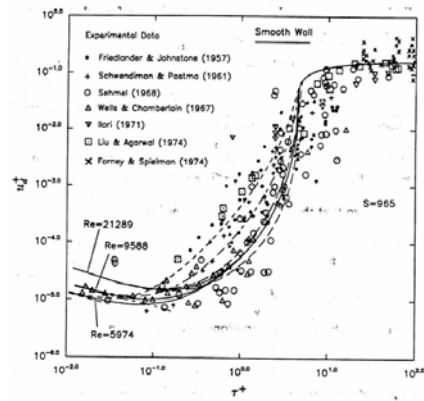
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Smooth Wall

Comparison with Experiments



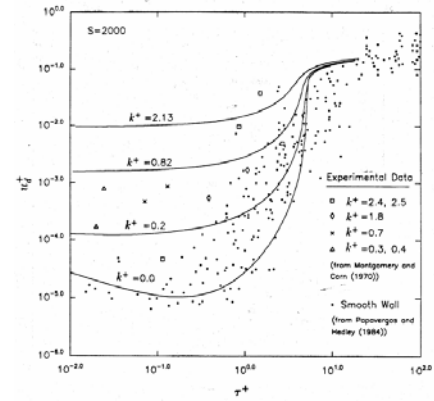
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Rough Wall

Comparison with Experiments



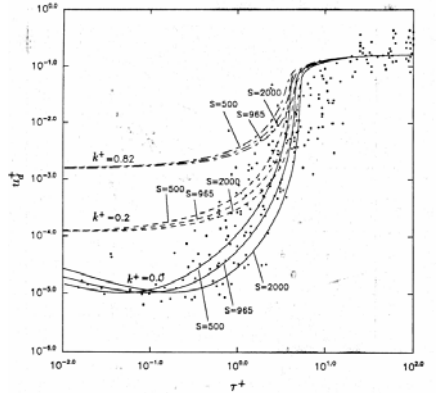
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Rough Wall

Effects of Density Ratio



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Deposition Velocity for Rough Walls Clarkson University

Fan and Ahmadi

Empirical Model

$$u_d^+ = \begin{cases} 0.084Sc^{-2/3} + \frac{1}{2} \left[\frac{(0.64k^+ + \frac{d^+}{2})^2 + \frac{\tau_p^{+2} g^+ L_1^+}{0.01085(1 + \tau_p^{+2} L_1^+)}}{3.42 + \frac{\tau_p^{+2} g^+ L_1^+}{0.01085(1 + \tau_p^{+2} L_1^+)}} \right]^{-1/(1 + \tau_p^{+2} L_1^+)} & \text{if } u_d^+ < 0.14 \\ \times \left[1 + 8e^{-(\tau_p^+ - 10)^2/32} \right] \frac{0.037}{1 - \tau_p^{+2} L_1^+ (1 + \frac{g^+}{0.037})} & \\ 0.14 & \text{otherwise} \end{cases}$$

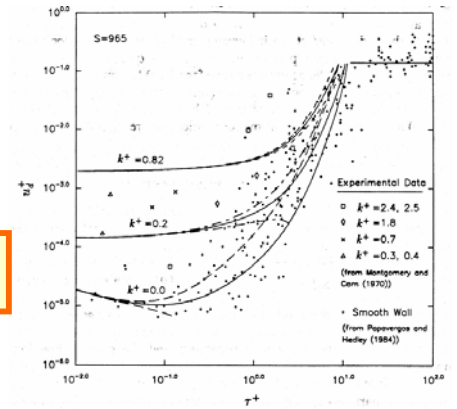
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Fan-Ahmadi Model Clarkson University

Rough Wall

Empirical Model Predictions



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Concluding Remarks Clarkson University

- ▶ **Semi-Empirical Models**
- ▶ **Free Flight Models**
- ▶ **Flow Structure Models**
- ▶ **Sublayer/Burst Models**
- ▶ **Deposition on Rough Walls**

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