

Particle Transport, Deposition and Removal

Clarkson
University

Review for Final Exam

Goodarz Ahmadi

Department of Mechanical and Aeronautical Engineering

Clarkson University

Potsdam, NY 13699-5725

Outline

- **Hydrodynamic Forces and Moments**
- **Diffusion Mechanisms**
- **Particle Adhesion and Detachment**
- **Particle Charging**

Hydrodynamic Forces

Drag Forces

$$F_D = \frac{3\pi\mu U d^f}{C_c} C_D$$

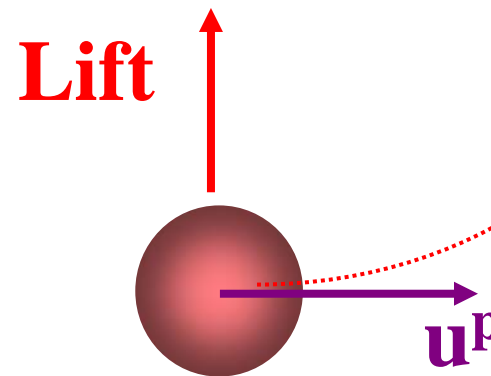
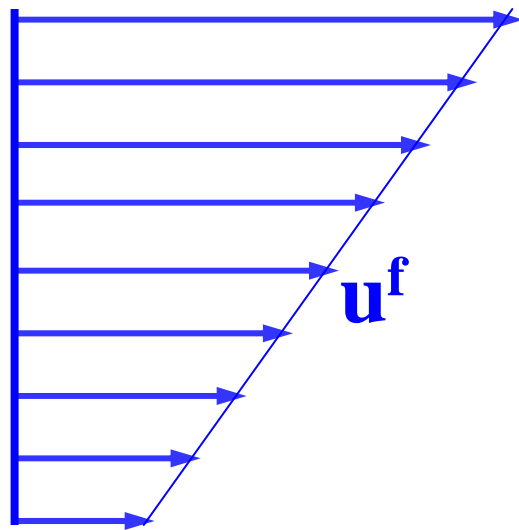
$$Re = \frac{\rho U d}{\mu}$$

$$C_D = \frac{24[1 + 0.15 Re^{0.687}]}{Re}$$

**Cunningham
Correction**

$$C_c = 1 + \frac{2\lambda}{d} [1.257 + 0.4e^{-1.1d/2\lambda}]$$

Lift Force

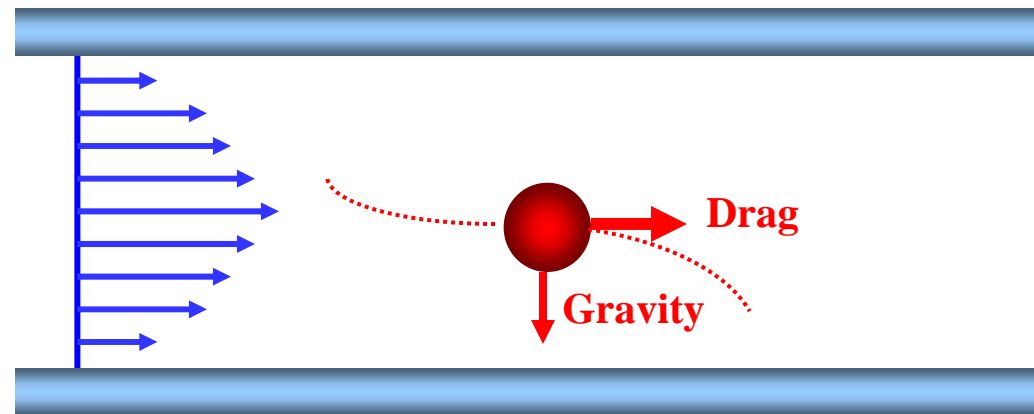


$$\text{sgn}(x) = \begin{cases} +1 & x > 0 \\ -1 & x < 0 \end{cases}$$

Saffman (1965, 1968)

$$F_{L(\text{Saff})} = 1.615 \rho v^{1/2} d^2 (u^f - u^p) \left| \frac{du^f}{dy} \right|^{1/2} \text{sgn}\left(\frac{du^f}{dy}\right)$$

Aerosols Particle Motion



Equation of Motion

$$m \frac{d\mathbf{u}^p}{dt} = \frac{3\pi\mu d}{C_c} (\mathbf{u}^f - \mathbf{u}^p) + m\mathbf{g}$$

Aerosols Particle Motion

$$\tau \frac{d\mathbf{u}^p}{dt} = (\mathbf{u}^f - \mathbf{u}^p) + \tau \mathbf{g}$$

Relaxation Time

$$\tau = \frac{mC_c}{3\pi\mu d} = \frac{d^2 \rho^p C_c}{18\mu} = \frac{Sd^2 C_c}{18\nu}$$

$$S = \frac{\rho^p}{\rho^f}$$

$$\tau(\text{s}) \approx 3 \times 10^{-6} d^2 (\mu\text{m})$$

Viscous Sublayer

Turbulent stress is negligible

$$\tau_0 = \mu \frac{dU}{dy}$$

$$u^{*2} = \nu \frac{dU}{dy}$$

$$\frac{dU^+}{dy^+} = 1$$

$$u = \frac{u^{*2} y}{\nu}$$

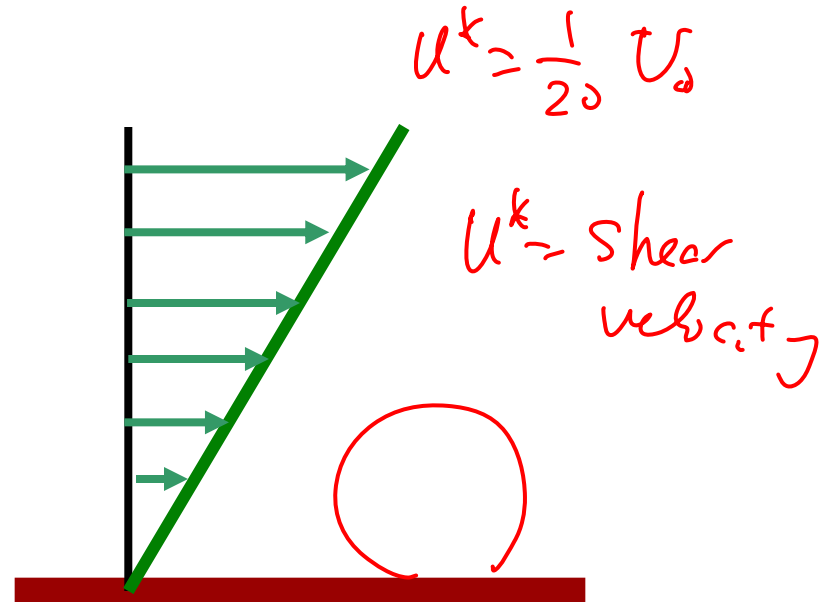
$$u^+ = y^+$$

$$0 < y^+ \leq 5$$

$$F^+ = \frac{F}{\mu \nu}$$

$$F_{L(Saff)}^+ = 0.807 d^{+3}$$

$$d^+ = \frac{d u^*}{\nu}$$



Diffusion and Fick's Law

Fick's Law

$$J = -D \frac{dc}{dx}$$

**Diffusion
Equation**

$$\frac{\partial c}{\partial t} + \mathbf{v} \cdot \nabla c = D \nabla^2 c$$

Diffusivity

$$D = \frac{kTC_c}{3\pi\mu d}$$

Diffusion

- **Similarity Method**
- **Separation of Variable Method**
- **Integral Method**

Particle Adhesion and Detachment

- **van der Waals Force**
- **JKR Adhesion Model**
- **DMT Adhesion Model**
- **Maugis-Pollock Model**
- **Particle Detachment Mechanisms**
- **Maximum Moment Resistance**

JKR Model

Johnson-Kandall-Roberts (1971)

$$a^3 = \frac{d}{2K} \left[P + \frac{3}{2} W_A \pi d + \sqrt{3\pi W_A d P + \left(\frac{3\pi W_A d}{2} \right)^2} \right]$$

$$K = \frac{4}{3} \left[\frac{1-\nu_1^2}{E_1} + \frac{1-\nu_2^2}{E_2} \right]^{-1}$$

Hertz Model

$$a^3 = \frac{dP}{2K}$$

DMT Model

Derjaguin-Muller-Toporov (1975)

Pull-Off Force

$$F_{Po}^{DMT} = \pi W_A d$$

$$F_{Po}^{DMT} = \frac{4}{3} F_{Po}^{JKR}$$

**Contact Radius
at Zero Force**

$$a_0 = \left(\frac{\pi W_A d^2}{2K} \right)^{\frac{1}{3}}$$

**Contact Radius at
Separation**

$$a = 0$$

Maugis-Pollock Model

$$P + \pi W_A d = \pi a^2 H$$

$$H = 3Y$$

$$a_0 \sim d^{\frac{2}{3}}$$



Elastic

$$a_0 \sim d^{\frac{1}{2}}$$



Plastic

JKR Model

$$a^{*3} = 1 - P^* + \sqrt{1 - 2P^*}$$

$$P^* = -\frac{P}{\frac{3}{2}\pi W_A d}$$

$$a^* = \frac{a}{\left(\frac{3\pi W_A d^2}{4K}\right)^{1/3}}$$

$$M^{*JKR} = P^* a^* = P^* (1 - P^* + \sqrt{1 - 2P^*})^{1/3}$$

$$M_{\max}^{*JKR} = 0.42$$

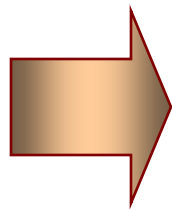
Aerosols Charging and Their Kinetics

Coulomb Force

$$\mathbf{F}_E = q\mathbf{E}$$

$$q = ne$$

Particle Mobility



$$u = Z^p = \frac{qC_c}{3\pi\mu d}$$

Particle Charging

Boltzmann Equilibrium Charge Distribution

$$f(n) = \frac{0.24}{\sqrt{d\pi}} \exp\left\{-\frac{0.05n^2}{d}\right\}$$

$$d > 0.02\mu\text{m}$$

$$\bar{n} \approx 2.36\sqrt{d}, \quad d(\mu\text{m})$$

Diffusion Charging

$$n = \frac{dkT}{2e^2} \ln \left[1 + \left(\frac{2\pi}{m_i kT} \right)^{1/2} n_{i\infty} de^2 t \right]$$

Field Charging

$$n_{\infty} = \left[1 + \frac{2(\epsilon_p - 1)}{\epsilon_p + 2} \right] \frac{Ed^2}{4e} \text{ as } t \rightarrow \infty$$

Problem 1

(40 points) Consider a steady convective-diffusion process with a flow velocity near an absorbing wall. The governing equation is given by

$$ay^2 \frac{\partial C}{\partial x} = D \frac{\partial^2 C}{\partial y^2}$$

where D is the diffusivity and a is a constant. The boundary conditions are:

$$C(x,0) = 0 \quad C(0,y) = C_0, \quad \text{and} \quad C(x,\infty) = C_0$$

i. Use a similarity variable, $\eta = \frac{y}{2(Dx/a)^{1/4}}$ reduce the governing

equation and boundary conditions to the similarity form.

ii. Evaluate the concentration profile and the deposition velocity to the wall.

$$ay^2 \frac{\partial C}{\partial X} = D \frac{\partial^2 C}{\partial y^2} \quad C = C(\eta)$$

$$\frac{x}{y^2} \sim y^2 \quad \left(\frac{y^4}{x}\right)^{1/4} \sim \eta \quad \boxed{\eta = \frac{y}{2(DX/a)^{1/4}}}$$

$$\frac{\partial C}{\partial y} = \frac{\partial C}{\partial \eta} \frac{\partial \eta}{\partial y} = \frac{\partial C}{\partial \eta} \left(\frac{1}{2(DX/a)^{1/4}} \right)$$

$$\frac{\partial^2 C}{\partial y^2} = \frac{\partial^2 C}{\partial \eta^2} \frac{1}{4(DX/a)^{1/2}}$$

$$\frac{\partial \eta}{\partial x} = \frac{y(-1/4)}{2(DX/a)^{1/4} X^{5/4}}$$

$$\frac{\partial C}{\partial x} = \frac{\partial C}{\partial \eta} \frac{\partial \eta}{\partial x} = \frac{\partial C}{\partial \eta} \left(-\frac{1}{4} \frac{\eta}{x} \right)$$

$$= -\frac{1}{4} \frac{\eta}{x}$$

$$\frac{\partial \eta}{\partial y} = \frac{1}{2(DX/a)^{1/4}}$$

$$ay^2 \left(-\frac{1}{4} \frac{\eta}{x} \right) \frac{\partial C}{\partial \eta} = D \frac{\partial^2 C}{\partial \eta^2} \frac{1}{4(DX/a)^{1/2}}$$

$$-\frac{ay^2}{x D} \eta \left(\frac{DX}{a} \right)^{1/2} \frac{\partial C}{\partial \eta} = \frac{\partial^2 C}{\partial \eta^2} \rightarrow \boxed{-4\eta^3 \frac{\partial C}{\partial \eta} = \frac{\partial^2 C}{\partial \eta^2}}$$

$$\frac{d^2 C}{d\eta^2} + 4\eta^3 \frac{dC}{d\eta} = 0 \quad C(0) = 0, \quad C(\infty) = C_0$$

$$\frac{\frac{d^2 C}{d\eta^2}}{\frac{dC}{d\eta}} = -4\eta^3 \rightarrow \ln \frac{dC}{d\eta} = -\eta^4 + \ln K$$

$$\frac{dC}{d\eta} = K e^{-\eta^4} \quad C(\infty) = 0$$

$$C = K \int_0^\eta e^{-\eta_1^4} d\eta_1 + A \xrightarrow{0}, \quad C_0 = K \int_0^\infty e^{-\eta_1^4} d\eta_1$$

$$C = C_0 \frac{\int_0^\eta e^{-\eta_1^4} d\eta_1}{\int_0^\infty e^{-\eta_1^4} d\eta_1}$$

$$J = D \frac{dC}{dy} \Big|_{y=0} = D \frac{dC}{d\eta} \Big|_{\eta=0} \frac{dy}{d\eta} = D \frac{C_0}{\int_0^\infty e^{-\eta_1^4} d\eta_1} \frac{1}{2(DX/a)^{1/4}}$$

$$U_d = \frac{J}{C_0} = \frac{D}{2 \left(\frac{Dx}{a}\right)^{1/4}} \frac{1}{\int_0^1 e^{-\eta^4} d\eta}$$

Problem 2

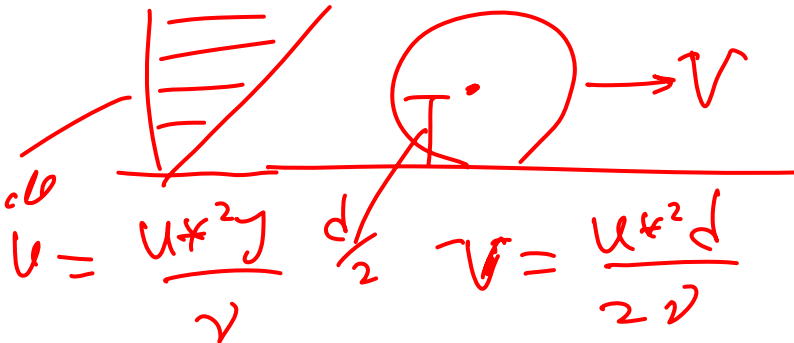
(35 points) Consider a 12 μm silicon particle that is attached to a silicon wafer in a turbulent air flow with a shear velocity of 2 m/s.

- i. Evaluate the drag, the Saffman lift and the hydrodynamic moment acting on the particle in wall units and in SI units.
- ii. Evaluate the pull-off force as predicted by the JKR model.
- iii. Find the contact radius at zero force and at the separation according to the JKR model.
- iv. Is the particle going to be removed by the rolling mechanism? (Assume $u^+ = y^+$, and for silicon use $W_A = 0.0389 \text{ J/m}^2$, $E = 1.79 \times 10^{11} \text{ N/m}^2$, and Poisson ratio of 0.27. The kinematic viscosity of air is $\nu = 1.5 \times 10^{-5} \text{ m}^2 / \text{s}$)

$$d = 12 \mu\text{m}, \quad U^* = 2 \text{ m/s}, \quad d^+ = \frac{d U^*}{\nu} = \frac{12 \times 10^{-6} \times 2}{1.5 \times 10^{-5}} = 1.6$$

$$F_t = \frac{3\pi \mu d V f}{C_c} \quad \left. \begin{array}{l} f = 1.7089 \\ \text{(Eq. 22)} \end{array} \right\}$$

$C_D = 1$ $Re - \text{small}$



$$F_t = \frac{3\pi(1.7)\mu d U^{*2} d}{2 \nu C_c}$$

$$= \frac{3\pi(1.7)\rho d^2 U^{*2}}{2 C_c} = \frac{2.9\pi \rho d^2 U^{*2}}{C_c} \quad (24)$$

$$U^+ = \frac{U^* d}{2\nu} \quad V^+ = \frac{U^* d}{2\nu}$$

$C_c = 1$ for $d = 12 \mu\text{m}$

$$F_t^+ = \frac{F_t}{\mu \nu} = 2.9\pi \frac{d^{+2}}{C_c} = 9.11 d^{+2} = \boxed{23.22}$$

$$F_t = \mu \nu F_t^+ = 1.2 (1.5 \times 10^{-5})^2 23.22 = \underline{\underline{6.297 \times 10^{-9} \text{ N}}}$$

$$\mu = \rho \nu \quad \left. \begin{array}{l} 1.2 \\ 1.2 \end{array} \right\}$$

Lift

$$F_L^+ = 0.807 d^{+3} = 3.31, \quad F_L = \mu \gamma F_L^+ = 8.92 \times 10^{-10} \text{ N}$$

$$M = 1.07 \pi \rho \frac{u^*{}^2 d^3}{c_c} \quad (\text{Eq. 30}) = 3.36 \rho u^*{}^2 d^3$$

$$M^+ = \frac{M}{\rho V \frac{3}{u^*}} = 3.36 d^{+3} = 13.77$$

$$M = 2.79 \times 10^{-14} \text{ N}\cdot\text{m}$$

$$\text{i)} \quad F_{p_0}^{7k1} = \frac{3\pi W_A d}{4} = \frac{3}{4} \pi (0.0389) 1.2 \times 10^{-5} = 1.1 \times 10^{-6} \text{ N}$$

$$\text{ii)} \quad K = \frac{4E}{3 \cdot 2(1-\nu^2)} = 1.287 \times 10^{11} \text{ N/m}^2$$

$$a_0 = \left(\frac{3\pi W_A d^2}{2K} \right)^{1/3} = 5.9 \times 10^{-8} \text{ m} = 0.059 \text{ } \mu\text{m}$$

$$a = a_0 / 4^{1/3} = 0.0372 \text{ } \mu\text{m}$$

$$IV) \quad F_D \frac{d}{2} + M_t + F_L a \stackrel{3.32 \times 10^{-17}}{=} M_{Max}^{JKR}$$

$$3.78 \times 10^{-14} \quad \downarrow \quad 2.79 \times 10^{-14} \quad \downarrow \quad 4.1 \times 10^{-14}$$

$$M^{Hydro} = 6.57 \times 10^{-14} > 4.1 \times 10^{-14} = M_{Max}^{JKR}$$

∴ Particle is Removed!

Problem 3

(25 points) Consider a cloud of $12 \mu\text{m}$ quartz particles with a concentration of 10^5 particles per cm^3 .

- i. Find the average absolute number of charge for the equilibrium Boltzmann distribution.
- ii. Determine the number of particles that will carry 5 positive charges. How many will carry no charges in this case?
- iii. Find the mean electrostatic precipitation velocity for a field of 400 Volt/cm for particles with the average absolute charge distribution.
- iv. Find the terminal velocity of these particles and compare with the electrostatic precipitation velocity.

(The density of air is 1.2 kg/m^3 , the density ratio of quartz particle to air is 2000, and charge of electron is $1.59 \times 10^{-19} \text{ Coul.}$)

$$d = 12 \mu\text{m}, \quad C_0 = 10^5 \text{ \#}/\text{cm}^3$$

$$\text{i) } \bar{n} = 2.36 \sqrt{d} = 2.36 \sqrt{12} = 8.17$$

$$\text{ii) } f(n) = \frac{0.24}{\sqrt{\pi d}} e^{-0.058 n^2/d} = 0.0391 e^{-0.00483 n^2}$$

$$f(0) = 0.0391 \quad N_0 = 3910$$

$$f(5) = 0.0346 \quad N_0 = 3460$$

$$\text{iii) } u = \frac{EgC_c}{3\pi\mu d}$$

$$U = \frac{40000 (8.17) (1.59 \times 10^{-19})}{3\pi (1.8 \times 10^{-5}) 1.2 \times 10^{-5}} = 2.55 \times 10^{-5} \frac{m}{s}$$

$$U = 25.5 \mu m/s$$

$$iv) \quad U_t = \tau g = \frac{5d^2 g}{18\eta} = \frac{2000 (12 \times 10^{-6})^2 \cdot 9.81}{18 (1.5 \times 10^{-5})}$$

$$U_t = 1.05 \times 10^{-2} m/s = 1.05 cm/s$$